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Explicit determination of the complex refractive index of an absorbing medium from reflectance measurements at and near normal incidence

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Measurement of reflectance at normal incidence R and its fractional change $\Delta R/R$ caused by a change of the angle of incidence from 0 to a small angle *φ (φ* ≲ 20°) permits explicit determination of both the refractive index *n* and extinction coefficient *k* of an isotropic absorbing medium. The medium of incidence (ambient) is assumed to have a known refractive index (e.g., =1 for vacuum or air), and the incident light is either *p* or *s* linearly polarized.

A variety of reflectance methods¹⁻¹² is available to determine the complex refractive index $N = n - jk$ of an absorbing medium. Few of those methods^{5,6,9,10} provide explicit solu tions for *n* and *k* in terms of the measured reflectances. In this Letter we propose a new method that provides simple, direct, and explicit determination of *n* and *k* in terms of the intensity reflectance measured at normal incidence *R* and the fractional change of such reflectance $\Delta \mathcal{R}/\mathcal{R}$ that results from a given change of angle of incidence from 0 to *φ,* where *φ* is a small angle (\lesssim 20°).

Figure 1 shows the normal-incidence reflection of light by the planar interface between a transparent ambient of known refractive index *N0* and an absorbing substrate (mirror) of complex refractive index N_1 to be determined. Both media are assumed to be homogeneous and isotropic. The mirror can be rotated about an axis *z* in its surface through the point of reflection by a known angle *φ.* The incident light is linearly polarized with its electric vector vibrating either parallel or perpendicular to the rotation axis. (These are the conventional *s* and p polarizations, respectively.) A complex reciprocal relative refractive index defined by

$$
N_r = N_0/N_1 = n_r + jk_r \tag{1}
$$

is more readily determined first by using the proposed method. Of course, once N_r is found, N_1 is given by

$$
N_1 = N_0/N_r = n_1 - jk_1.
$$
 (2)

The signs of the imaginary parts in Eqs. (1) and (2) are consistent with the Nebraska (Muller) conventions.¹³

The first equation to be used is¹⁴

$$
\frac{\Delta r_{\nu}}{r_{\nu}} = \pm N_r \phi^2,\tag{3}
$$

which gives the fractional change of Fresnel's complex interface reflection coefficient for the *v* polarization (+ for *v = s* and $-$ for ν = p) that results from changing the angle of incidence from 0 to ϕ , where ϕ is a given small angle. The measurable fractional change of intensity reflectance, *∆Rv /Rv,* is related to $\Delta r_{\nu}/r_{\nu}$ by

$$
\Delta \mathcal{R}_{\nu} / \mathcal{R}_{\nu} = 2 \operatorname{Re}(\Delta r_{\nu} / r_{\nu}), \tag{4}
$$

where Re means the real part of. Substitution of Eq. (3) into Eq. (4) and use of Eq. (1) give

$$
|\Delta \mathcal{R}_{\nu}/\mathcal{R}_{\nu}| = 2n_r\phi^2. \tag{5}
$$

Equation (5) readily determines *nr:*

$$
n_r = \left| \Delta \mathcal{R}_\nu / \mathcal{R}_\nu \right| / 2\phi^2. \tag{6}
$$

 $(\text{If } |\Delta \mathcal{R}_{\nu} / \mathcal{R}_{\nu}|)$, measured at various values of small ϕ , is plotted versus $2\phi^2$, the slope of the resulting straight line gives a precise estimate of n_r .) Subsequently, k_r is found from the normal-incidence reflectance

$$
\mathcal{R}_r = |(1 - N_r)/(1 + N_r)|^2 \tag{7}
$$

or

$$
\mathcal{R}_{\nu} = \left[(1 - n_r)^2 + k_r^2 \right] / \left[(1 + n_r)^2 + k_r^2 \right]. \tag{8}
$$

Equation (8) gives

$$
k_r = \left[2n_r\left(\frac{1+\mathcal{R}_\nu}{1-\mathcal{R}_\nu}\right) - (n_r^2+1)\right]^{1/2}.\tag{9}
$$

Equations (6) and (9) show explicitly how the complex reciprocal relative refractive index, $N_r = n_r + j k_r$, is determined from the normal-incidence reflectance *R* and its fractional change *∆R/R* caused by changing incidence from normal to a small angle *φ.* The substrate complex refractive index *N¹* is calculated from N_r and the known refractive index N_0 of the ambient (usually air, $N_0 = 1$) by using Eq. (2).

The incident light is assumed to be either p or *s* polarized. The method in its present form would not work if the incident light were unpolarized. This is because $\Delta \mathcal{R}_p / \mathcal{R}_p$ = $-\Delta \mathcal{R}_s/\mathcal{R}_s$, so that

$$
\Delta \mathcal{R}_u / \mathcal{R}_u = 0 \tag{10}
$$

to second order in *φ* (the subscript *u* denotes unpolarized).

 $\Delta R/R$ can be accurately determined by a lock-in technique if the mirror is periodically oscillated (e.g., sinusoidally, so that $\phi = \hat{\phi}$ sin ωt , where $\hat{\phi}$ is a small-amplitude angular excursion) and the modulation of the reflected light intensity *∆I/I* is

Fig. 1. Normal-incidence reflection of light by the interface between a transparent ambient of known refractive index N_0 and an absorbing substrate (mirror) with unknown complex refractive index *N1.* The mirror can be rotated around an axis *z* in its surface through the point of reflection. p and s are linear-polarization directions perpendicular and parallel to the rotation axis, respectively.

determined. With the intensity of the incident light constant, it is easy to show that

$$
\Delta \mathcal{R}/\mathcal{R} = \Delta I/I. \tag{11}
$$

The method can be considered as an interesting special case of angle-of-incidence derivative ellipsometry and reflectometry^{15,16} and, more closely, of a method previously described by Hunderi.¹⁷

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